# Power MOSFET Integrated High Efficiency BCM LED Driver Controller for High Power Factor Applications

## General Description

The RT8497 integrates a power MOSFET and a Boundary mode controller. It is used for step down converters by well controlling the internal MOSFET and regulating a constant output current.

The RT8497 features a ZCS detector which keeps system operating in BCM and obtaining excellent power efficiency, better EMI performance.

The RT8497 achieves high Power Factor Correction (PFC) and low Total Harmonic Distortion of Current (THDi) by a smart internal line voltage compensation circuit which has minimized system component counts; saved both PCB size and total system cost.

Especially, the RT8497 can use a cheap simple drum core inductor in the system instead of an EE core to obtain high efficiency.

The RT8497 is housed in a SOP-8 package. Thus, the components in the whole LED driver system can be made very compact.

## Ordering Information

RT8497 □□□

- Package Type
  S : SOP-8
- Lead Plating System
  G : Green (Halogen Free and Pb Free)
- MOSFET Built-In
  Default : 500V/5.2Ω
  A : 500V/2Ω
  B : 600V/4.2Ω
  C : 600V/7Ω
  D : 600/3.2Ω

Note :

Richtek products are :

- RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- Suitable for use in SnPb or Pb-free soldering processes

## Features

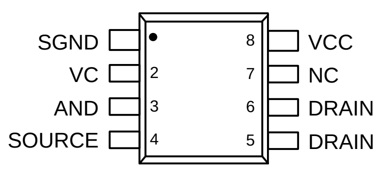
- **Built-In Power MOSFET**
- **Support High Power Factor and Low THDi Applications**
- **Programmable Constant LED Current with High-Precision Current Regulation**
- **Extremely Low Quiescent Current Consumption and 1μA Shutdown Current**
- **Compact Floating Buck Topology with Low Component Counts, Small PCB Size, and Low System BOM Cost**
- **Unique Programmable AND Pin for ZVS Setting to Achieve Best Power Efficiency**
- **Support Off-Line Universal Input Voltage Range**
- **Built-in Over Thermal Protection**
- **Built-in Over Voltage Protection**
- **Output LED String Open Protection**
- **Output LED String Short Protection**
- **Output LED String Over Current Protection**

## Applications

- E27, PAR, Light Bar, Offline LED Lights

## Pin Configuration

(TOP VIEW)




SOP-8

## Marking Information

RT8497GS

RT8497
GSYMDNN

RT8497GS : Product Number
YMDNN : Date Code

RT8497AGS

RT8497A
GSYMDNN

RT8497AGS : Product Number
YMDNN : Date Code

RT8497BGS

RT8497B
GSYMDNN

RT8497BGS : Product Number
YMDNN : Date Code

RT8497CGS

RT8497C
GSYMDNN

RT8497CGS : Product Number
YMDNN : Date Code

RT8497DGS

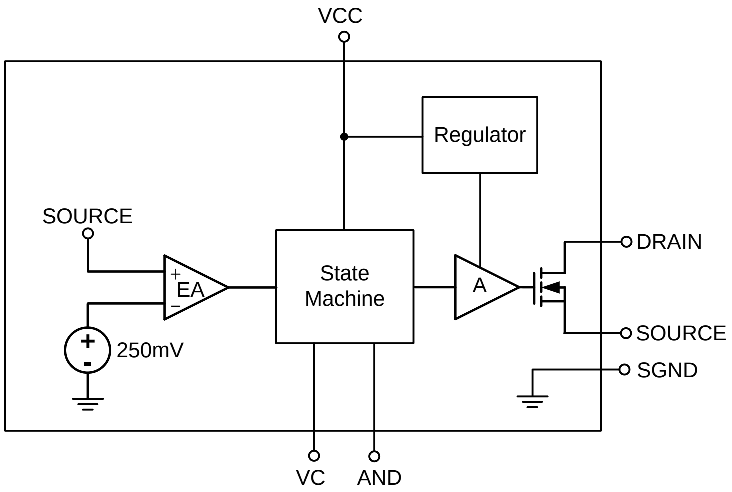
RT8497D
GSYMDNN

RT8497DGS : Product Number
YMDNN : Date Code

## Functional Pin Description

| Pin No. | Pin Name | Pin Function |
|---|---|---|
| 1 | SGND | Ground of the chip. |
| 2 | VC | Close Loop compensation node. |
| 3 | AND | Next delay timing function control. |
| 4 | SOURCE | Internal power MOSFET source connection. |
| 5, 6 | DRAIN | Internal power MOSFET drain connection. |
| 7 | NC | No internal connection. |
| 8 | VCC | Supply voltage input of the chip. For good bypass, a ceramic capacitor near the VCC pin is required. |

## Functional Block Diagram




## Operation

The RT8497 senses true average output current and keeps the system driving constant output current. The VC pin is the compensation node in this close loop system and dominates the frequency response. To stabilize the system and achieve better PFC / THDi, proper selection of a compensation network is needed.

## Absolute Maximum Ratings (Note 1)

- Supply Input Voltage ---------- –0.3V to 40V
- DRAIN to SOURCE Voltage, $V_{DS}$, (RT8497B, RT8497C, RT8497D) ---------- –0.3V to 600V
- DRAIN to SOURCE Voltage, $V_{DS}$, (RT8497, RT8497A) ---------- –0.3V to 500V
- DRAIN Current, $I_D$ @ $T_C$ = 25°C ---------- 1.4A
- DRAIN Current, $I_D$ @ $T_C$ = 100°C ---------- 0.9A
- Power Dissipation, $P_D$ @ $T_A$ = 25°C
  SOP-8 ---------- 0.53W
- Package Thermal Resistance (Note 2)
  SOP-8, $\theta_{JA}$ ---------- 188°C/W
- Lead Temperature (Soldering, 10 sec.) ---------- 260°C
- Junction Temperature ---------- 150°C
- Storage Temperature Range ---------- –65°C to 150°C
- ESD Susceptibility (Note 3)
  HBM (Human Body Model) ---------- 2kV

## Recommended Operating Conditions (Note 4)

- Supply Input Voltage ---------- 10V to 30V
- Ambient Temperature Range ---------- –40°C to 85°C
- Junction Temperature Range ---------- –40°C to 125°C

## Electrical Characteristics

($V_{CC}$ = 24V, $T_A$ = 25°C, unless otherwise specified)

| Parameter | Symbol | Test Conditions | | Min | Typ | Max | Unit |
|---|---|---|---|---|---|---|---|
| VCC UVLO ON | $V_{UVLO\_ON}$ | | | 17 | 18 | 19 | V |
| VCC UVLO OFF | $V_{UVLO\_OFF}$ | | | 6.4 | 7.2 | 8 | V |
| VCC Shut Down Current | $I_{SHDN}$ | $V_{CC}$ = 15V | | -- | -- | 1 | μA |
| VCC Quiescent Current | $I_Q$ | Drain stands still | | -- | 0.5 | 5 | mA |
| VCC Operating Current | $I_{CC}$ | By $C_{GATE}$ = 1nF, Freq. = 20kHz | | -- | 1 | 5 | mA |
| VCC OVP Level | $V_{OVP}$ | | | 31.5 | 34 | 38.5 | V |
| Current Sense Threshold | $V_{SENSE}$ | | | 242.5 | 250 | 257.5 | mV |
| AND Pin Leakage Current | $I_{AND}$ | $V_{AND}$ = 5V | | -- | 1 | 2 | μA |
| Static Drain-Source On-Resistance | $R_{DS(ON)}$ | $V_{GS}$ = 12V, $I_D$ = 100mA | RT8497 | -- | 5.2 | -- | Ω |
| | | | RT8497A | -- | 2 | -- | |
| | | | RT8497B | -- | 4.2 | -- | |
| | | | RT8497C | -- | 7 | -- | |
| | | | RT8497D | -- | 3.2 | -- | |

| Parameter | Symbol | Test Conditions | Min | Typ | Max | Unit |
|---|---|---|---|---|---|---|
| Drain-Source Leakage Current | $I_{DSS}$ | RT8497, $V_{DS}$ = 500V | -- | -- | 10 | μA |
| | | RT8497A, $V_{DS}$ = 500V | | | | |
| | | RT8497B, $V_{DS}$ = 600V | | | | |
| | | RT8497C, $V_{DS}$ = 600V | | | | |
| | | RT8497D, $V_{DS}$ = 600V | | | | |

**Note 1.** Stresses beyond those listed "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

**Note 2.** $\theta_{JA}$ is measured under natural convection (still air) at $T_A$ = 25°C with the component mounted on a high effective-thermal-conductivity four-layer test board on a JEDEC 51-7 thermal measurement standard.

**Note 3.** Devices are ESD sensitive. Handling precaution recommended.

**Note 4.** The device is not guaranteed to function outside its operating conditions

## Typical Application Circuit

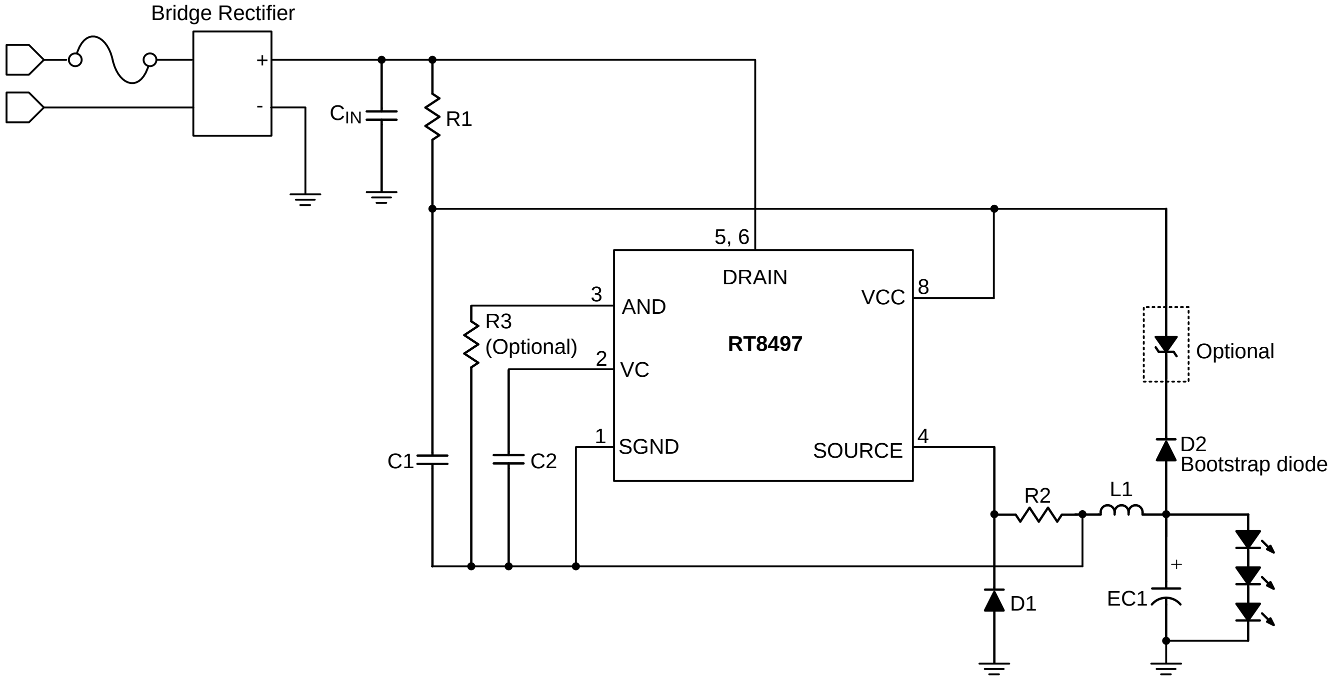
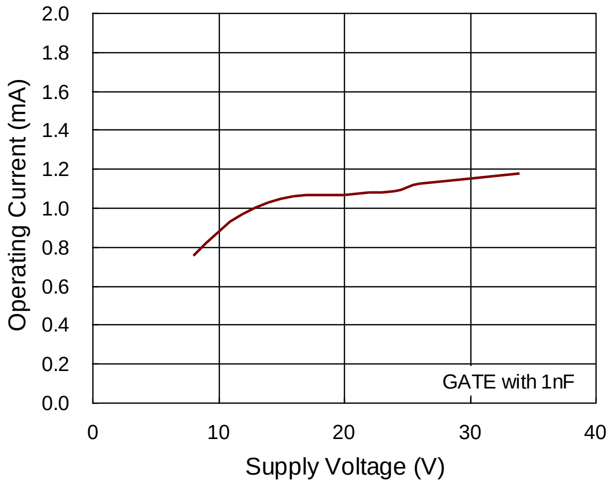


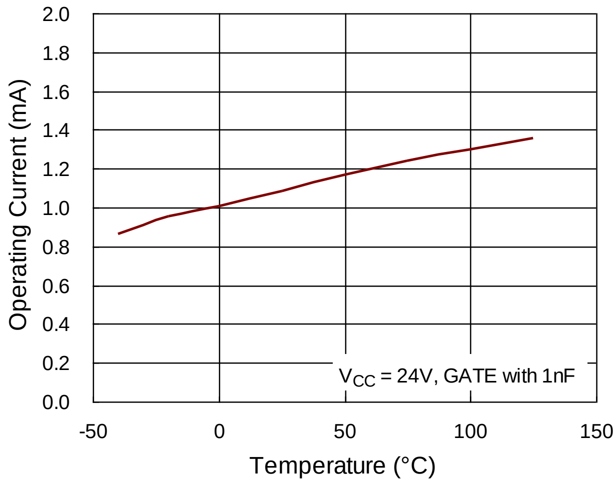

Figure 1. Typical Application of Buck Type

## Typical Operating Characteristics

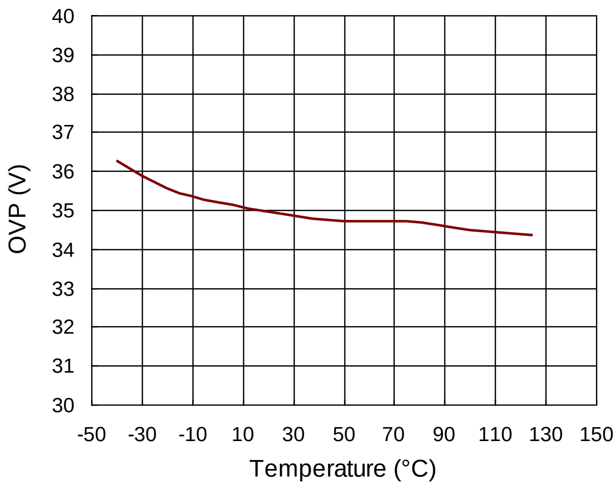
Operating Current vs. Supply Voltage



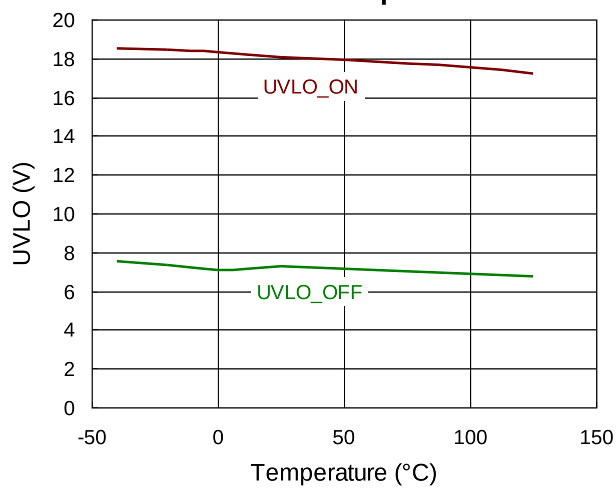

Operating Current vs. Temperature



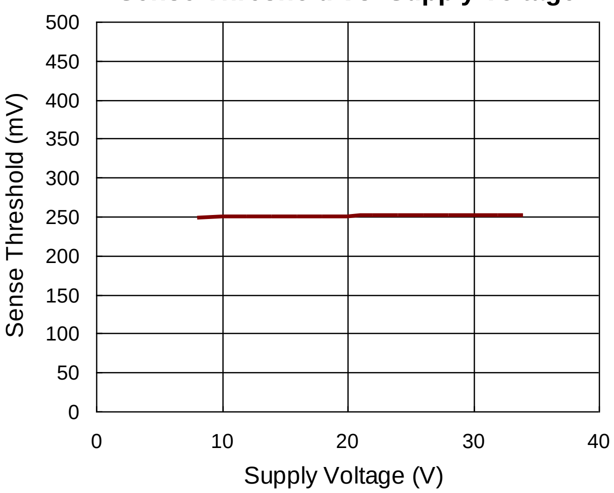

OVP vs. Temperature



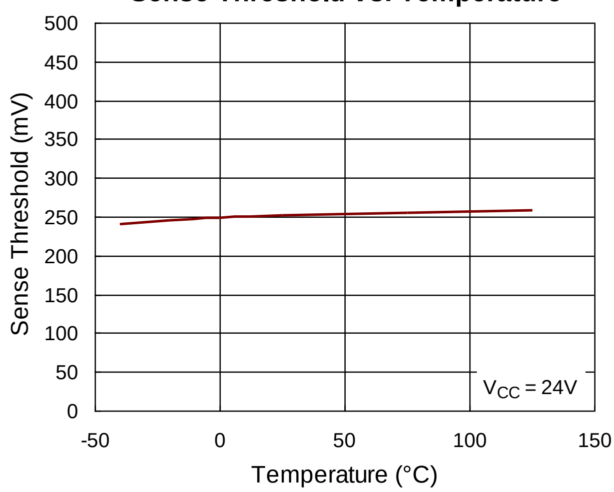

UVLO vs. Temperature



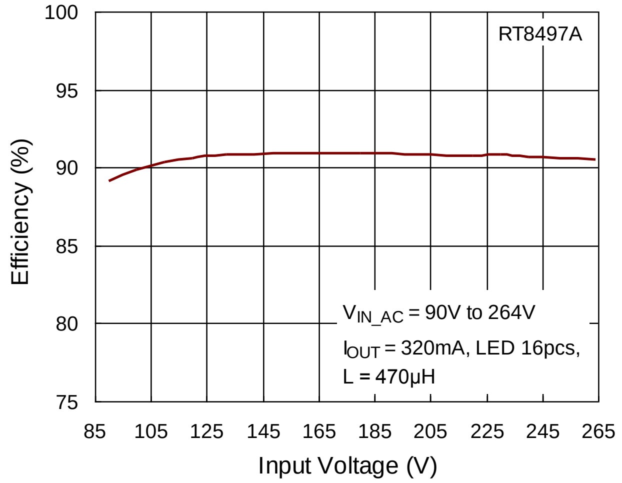

Sense Threshold vs. Supply Voltage



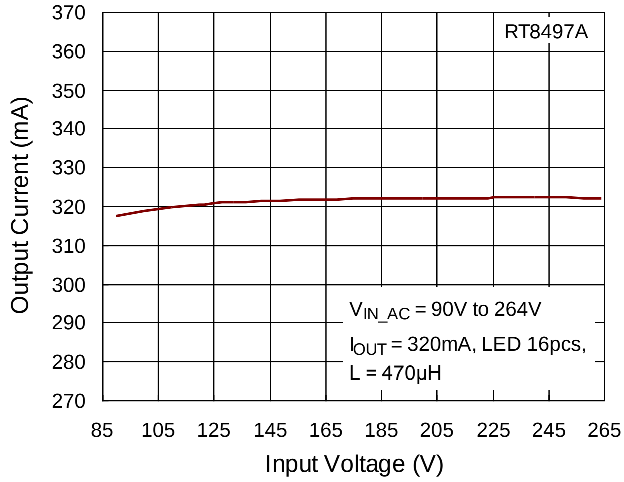

Sense Threshold vs. Temperature



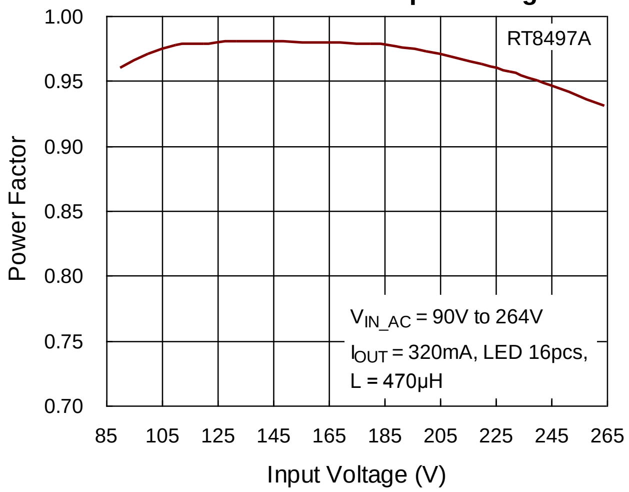
**Efficiency vs. Input Voltage**



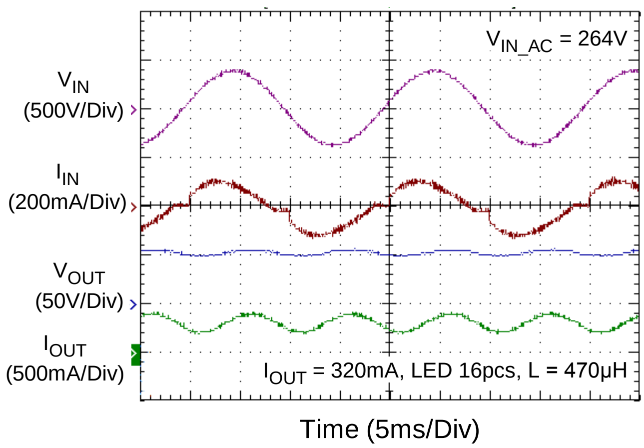

**Output Current vs. Input Voltage**



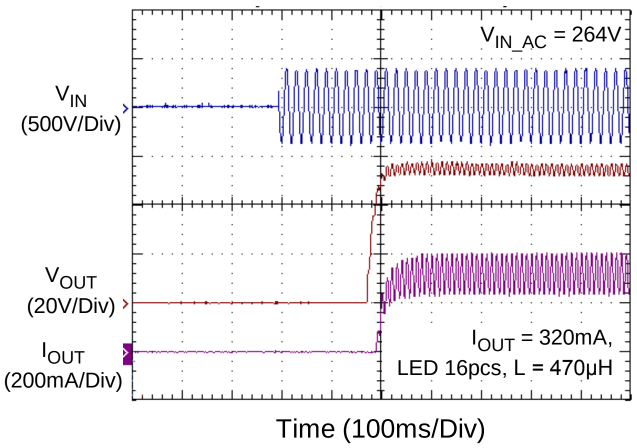

**Power Factor vs. Input Voltage**



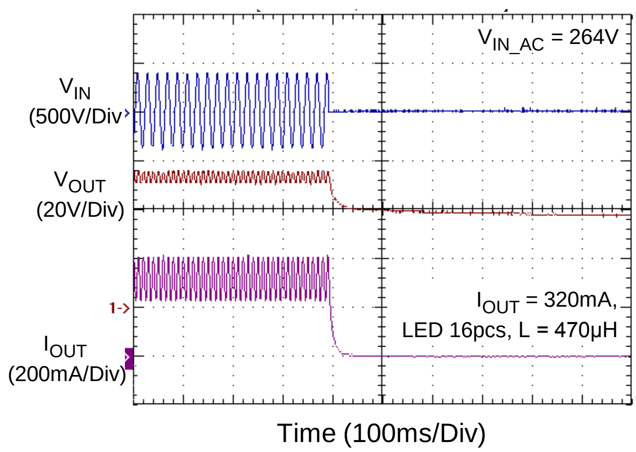

**Input and Output Current**

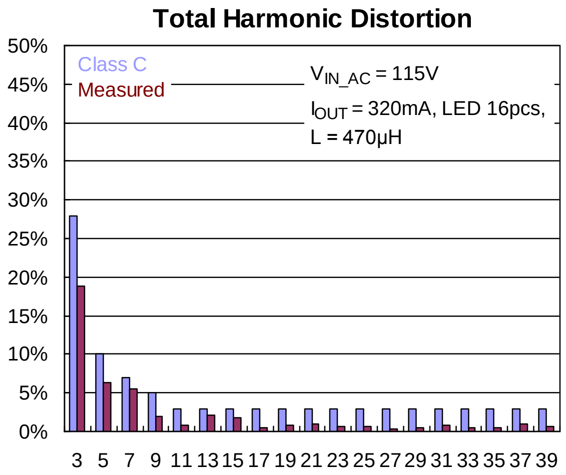


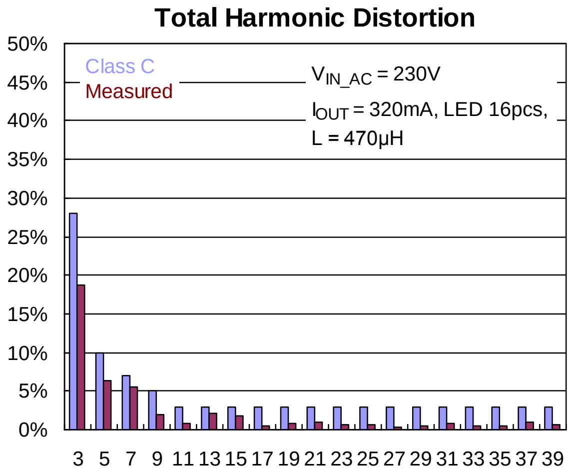

**Power On**




**Power Off**




Total Harmonic Distortion
Class C
Measured
VIN_AC = 115V
IOUT = 320mA, LED 16pcs,
L = 470μH
50%
45%
40%
35%
30%
25%
20%
15%
10%
5%
0%
3 5 7 9 11 13 15 17 19 21 23 25 27 29 31 33 35 37 39


Total Harmonic Distortion
Class C
Measured
VIN_AC = 230V
IOUT = 320mA, LED 16pcs,
L = 470μH
50%
45%
40%
35%
30%
25%
20%
15%
10%
5%
0%
3 5 7 9 11 13 15 17 19 21 23 25 27 29 31 33 35 37 39

## Application Information

The RT8497 is a Boundary mode converter, which can be used in buck configuration, to provide a constant output current to the (LED) load. It contains special circuitry for achieving high power factor and low input current THD, while minimizing external component count. The RT8497 integrates a power MOSFET and housed in a SOP-8 package. Thus, the components in the whole LED driver system can be made very compact.

The RT8497 can achieve high accuracy LED output current via the average current feedback loop control. The internal sense voltage (250mV typ.) is used to set the average output current. The average current is set by the external resistor, RS. The sense voltage is also used for over current protection (OCP) function. The typical OCP threshold is about seven times of the sense voltage threshold.

### Under Voltage Lockout (UVLO)

The RT8497 includes a UVLO function with 10.8V hysteresis. For system start up, the VIN must rise over 18V (typ.) to turn on the internal MOSFET. The internal MOSFET will turn off if VIN falls below 7.2V (typ.)

### Setting Average Output Current

The output current that flows through the LED string is set by an external resistor, RS, which is connected between the GND and SOURCE pins. The relationship between output current, $I_{OUT}$, and RS is shown below :

$$I_{OUT} = \frac{250}{R_S}(\text{mA})$$

### Start-up Resistor

The start-up resistor should be chosen to set the start up current exceeds certain minimum value. Otherwise, the RT8497 may latch off and the system will never start.

The start-up current equals $\left(\sqrt{2}\times 90V\right)$ / (R1 +R2) (for 110VAC regions), and equals $\left(\sqrt{2}\times 180V\right)$ / (R1 +R2) (for 220VAC regions). The typical required minimum start-up current is 100μA. The typical total start up resistance (R1+ R2) is around 1M Ohm for universal inputs.

### Input Diode Bridge Rectifier Selection

The current rating of the input bridge rectifier is dependent on the $V_{OUT}$ /$V_{IN}$ conversion ratio and out LED current. The voltage rating of the input bridge rectifier, $V_{BR}$, on the other hand, is only dependent on the input voltage. Thus, the VBR rating is calculated as below :

$$V_{BR} = 1.2\times\left(\sqrt{2}\times V_{AC(MAX)}\right)$$

where $V_{AC(MAX)}$ is the maximum input voltage (RMS) and the parameter 1.2 is used for safety margin.

For this example :

$$V_{BR} = 1.2\times\left(\sqrt{2}\times V_{AC(MAX)}\right) = \left(1.2\times\sqrt{2}\times 264\right) = 448V$$

If the input source is universal, $V_{BR}$ will reach 448V. In this case, a 600V, 0.5A bridge rectifier can be chosen.

### Input Capacitor Selection

For High Power Factor application, the input Capacitor CIN should use a small value capacitance to achieve line voltage sine-wave.

The voltage rating of the input filter capacitor, $V_{CIN}$, should be large enough to handle the input voltage. $V_{CIN} \geq (1.2\times 2 \times V_{AC(MAX)}) = (1.2\times 2 \times 264) = 448V$ Thus, a 0.1μF / 500V film capacitor can be chosen in this case.

### Inductor Selection

For high power factor application, the RT8497 operates the converter in BCM (Boundary-Condition Mode). The inductance range is defined by peak current of inductor、maximum and minimum value of switching on time and off time, for ensuring the inductor operates in BCM. The peak current of inductor is showed as below :

$$I_{PEAK} = \frac{2Pin}{V_{PEAK}F(a)}$$

$$\text{where } a = \frac{V_{OUT}}{V_{PEAK}}$$

and

$$F(a) \approx -0.411a^4+0.296a^3-0.312a^2+0.638a-0.0000846, \{a|0\sim0.7\}$$

The inductance range is showed as below :

$$L = \frac{V_{OUT} T_{OFF}}{I_{PEAK}} = \frac{(V_{PEAK} - V_{OUT}) T_{ON}}{I_{PEAK}}$$

Where $0.5\mu s \leq T_{ON} \leq 35\mu s$ and $2\mu s \leq T_{OFF} \leq 30\mu s$

The frequency at the top of the sine wave can be calculated :

$$f_{SW} = \frac{1}{T_{ON} + T_{OFF} + T_{DELAY}}$$

($T_{delay}$ is determined by the resistor connected to AND pin , see Turn on delay time)

### Turn On Delay Time

After the inductor current has reached zero, a resonance will occur between the inductor and the MOSFET drain-source capacitance.

In order to minimize the MOSFET switching losses, the RT8497 provides the flexibility to adjust the delay time of next switch-on cycle in order to switch-on at the maximum point of the resonance, which corresponds to the minimum drain-source voltage value.

The delay time from zero current point to the maximum of the switch resonance which can be calculated from :

$$T_{resonance} = \pi\sqrt{L1 \times C_{SW}}$$

where $C_{SW}$ is the capacitance at the switch node, mostly determined by the MOSFET drain-source capacitance.

The delay time $T_{DELAY}$ from zero current detection point to next MOSFET switch-on cycle can be adjusted by the resistor value R3B connected between AND pin and IC GND

$$T_{DELAY}(\mu s) = (-0.4 \text{ x } R3B^2 + 3500 \text{ x } R3B + 407500) \text{ x } 10^{-6}$$

R3B resister value in kΩ.

### Forward Diode Selection

When the power switch turns off, the path for the current is through the diode connected between the switch output and ground. This forward biased diode must have minimum voltage drop and recovery time. The reverse voltage rating of the diode should be greater than the maximum input voltage and the current rating should be greater than the maximum load current.

The peak voltage stress of diode is :

$$V_D \geq 1.2 \times (\sqrt{2} \times V_{AC(MAX)}) = 1.2 \times (\sqrt{2} \times 264) = 448V$$

The input source is universal ($V_{IN}$ = 85V to 264V), $V_D$ will reach 448V.

### Thermal Protection (OTP)

A thermal protection feature is included to protect the RT8497 from excessive heat damage. When the junction temperature exceeds a threshold of 150°C, the thermal protection OTP will be triggered and the internal MOSFET will be turned off.

### Thermal Considerations

The junction temperature should never exceed the absolute maximum junction temperature $T_{J(MAX)}$, listed under Absolute Maximum Ratings, to avoid permanent damage to the device. The maximum allowable power dissipation depends on the thermal resistance of the IC package, the PCB layout, the rate of surrounding airflow, and the difference between the junction and ambient temperatures. The maximum power dissipation can be calculated using the following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

where $T_{J(MAX)}$ is the maximum junction temperature, $T_A$ is the ambient temperature, and $\theta_{JA}$ is the junction-to-ambient thermal resistance.

For continuous operation, the maximum operating junction temperature indicated under Recommended Operating Conditions is 125°C. The junction-to-ambient thermal resistance, $\theta_{JA}$, is highly package dependent. For a SOP-8 package, the thermal resistance, $\theta_{JA}$, is 188°C/W on a standard JEDEC 51-7 high effective-thermal-conductivity four-layer test board. The maximum power dissipation at $T_A$ = 25°C can be calculated as below :

$P_{D(MAX)}$ = (125°C − 25°C) / (188°C/W) = 0.53W for a SOP-8 package.

The maximum power dissipation depends on the operating ambient temperature for the fixed $T_{J(MAX)}$ and the thermal resistance, $\theta_{JA}$. The derating curves in Figure 2 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.

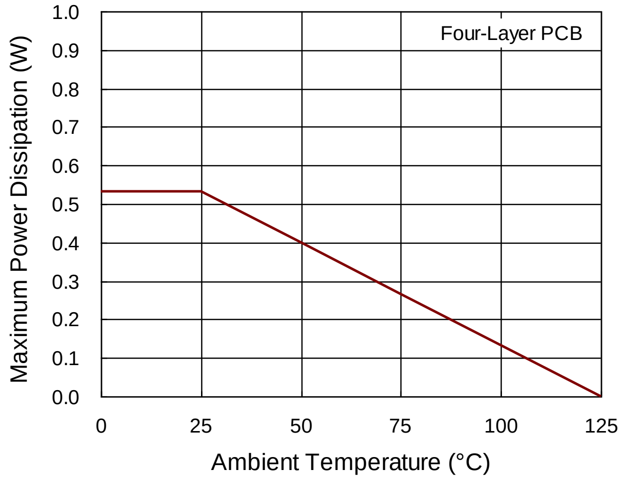



Figure 2. Derating Curve of Maximum Power Dissipation

### Layout Considerations

For best performance of the RT8497, the following layout guidelines should be strictly followed.

The hold up capacitor, C1, must be placed as close as possible to the VCC pin.

The compensation capacitor, C2, and delay resistor, R3B, must be placed as close as possible to the VC and the AND pin.

The IC SOURCE pin are high frequency switching nodes. The traces must be as wide and short as possible.

Keep the main traces with switching current as short and wide as possible.

Place $C_{IN}$, L1, RS, $C_{OUT}$, and D1 as close to each other as possible.

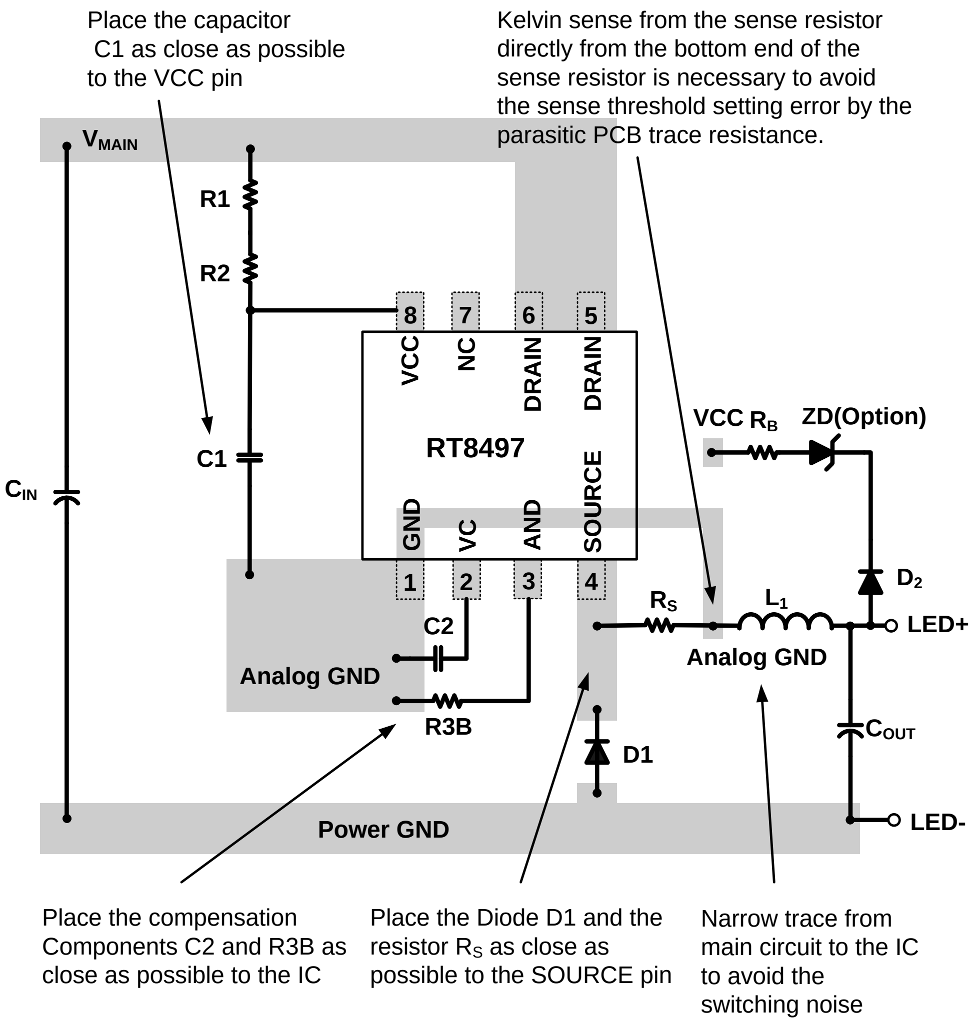
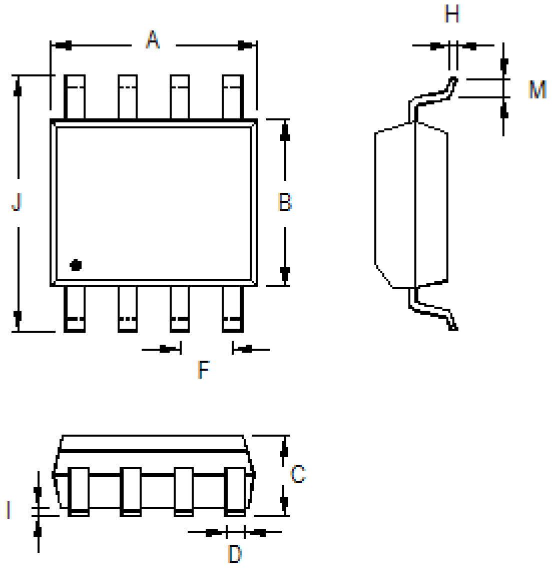



Figure 3. PCB Layout Guide

## Outline Dimension




| Symbol | Dimensions In Millimeters | | Dimensions In Inches | |
|---|---|---|---|---|
| | Min | Max | Min | Max |
| A | 4.801 | 5.004 | 0.189 | 0.197 |
| B | 3.810 | 3.988 | 0.150 | 0.157 |
| C | 1.346 | 1.753 | 0.053 | 0.069 |
| D | 0.330 | 0.508 | 0.013 | 0.020 |
| F | 1.194 | 1.346 | 0.047 | 0.053 |
| H | 0.170 | 0.254 | 0.007 | 0.010 |
| I | 0.050 | 0.254 | 0.002 | 0.010 |
| J | 5.791 | 6.200 | 0.228 | 0.244 |
| M | 0.400 | 1.270 | 0.016 | 0.050 |

**8-Lead SOP Plastic Package**

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